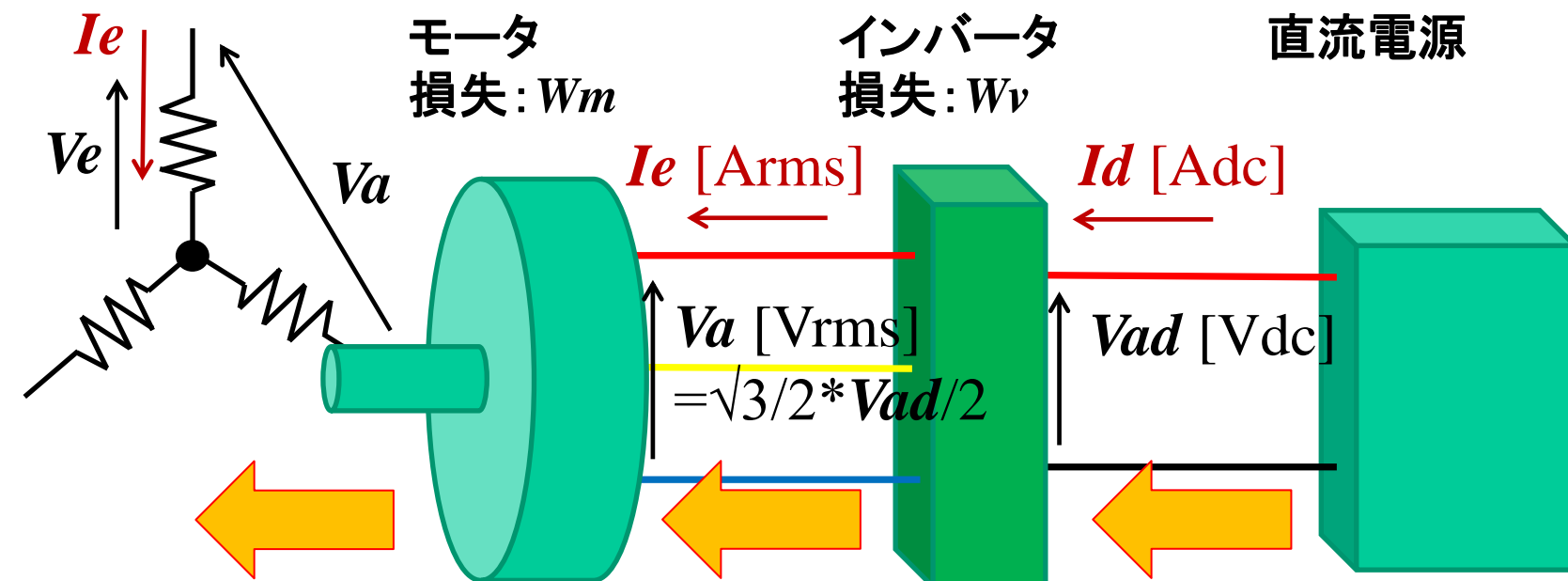


# 交流直流変換における定数



出力:  $P_{out} = T * \omega$

$$P_{in} = P_{out} + W_m$$

$$= \sqrt{3} * V_a * I_e * \cos\phi = 3 * V_e * I_e * \cos\phi$$

$$= \frac{3}{(2\sqrt{2})} V_{ad} * I_e * \cos\phi$$

$$P_d = P_{in} + W_v$$

$$= I_d * V_{ad}$$

いま、 $W_v \doteq 0$  ( $P_{in} = P_d$ ),  $\cos\phi \doteq 1$  とすれば

誘起電圧定数:  $K_e = V_e / N = 1 / (2\sqrt{2}) * V_{ad} / N = 1 / (2\sqrt{2}) * K_{ed}$

$$K_{ed} = V_{ad} / N$$

トルク定数:  $K_t = T / I_e = (2\sqrt{2}) / 3 * T / I_d \doteq 0.94 * K_{td}$

$$K_{td} = T / I_d$$

効率:  $\eta = P_{out} / P_{in}$

$$\eta_d = P_{out} / P_d$$

# 3相PWMインバータの構成

正弦波の場合：

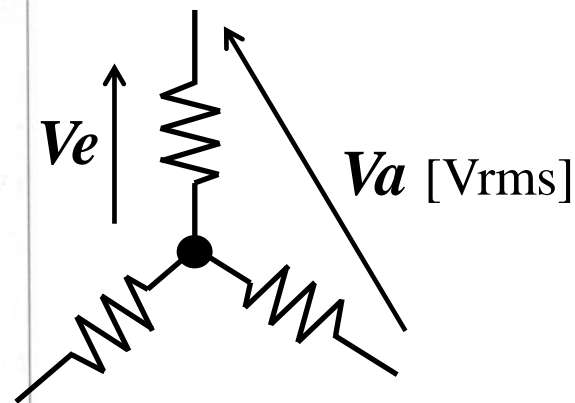
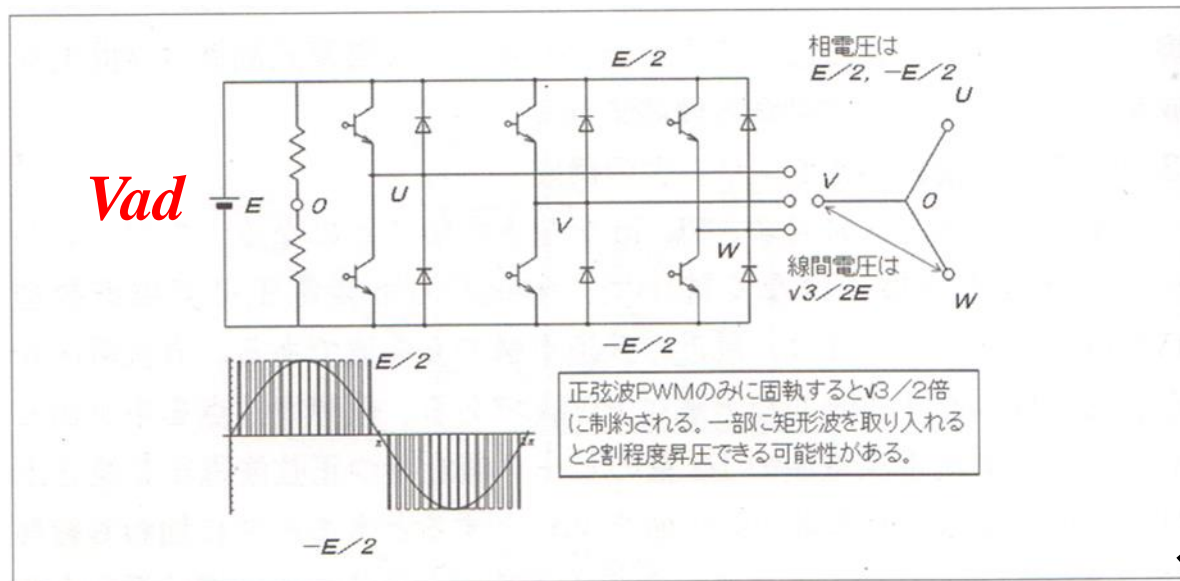
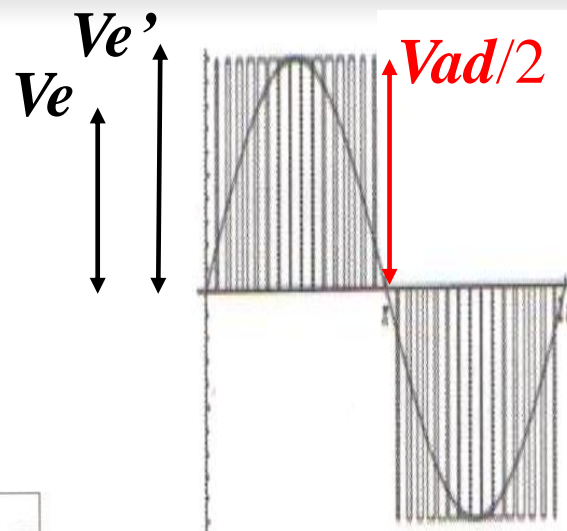
$$V_e [\text{Vrms}] = 1/\sqrt{2} * V_{ad} [\text{Vdc}]/2$$

$$V_a [\text{Vrms}] = \sqrt{3} * V_e = \sqrt{3}/(2\sqrt{2}) * V_{ad} [\text{Vdc}]$$

矩形波の場合 (180° 通電、過変調制御等)：

$$V_e' [\text{Vrms}] = V_{ad} [\text{Vdc}]/2$$

$$V_a' [\text{Vrms}] = \sqrt{3}/2 * V_{ad} [\text{Vdc}]$$



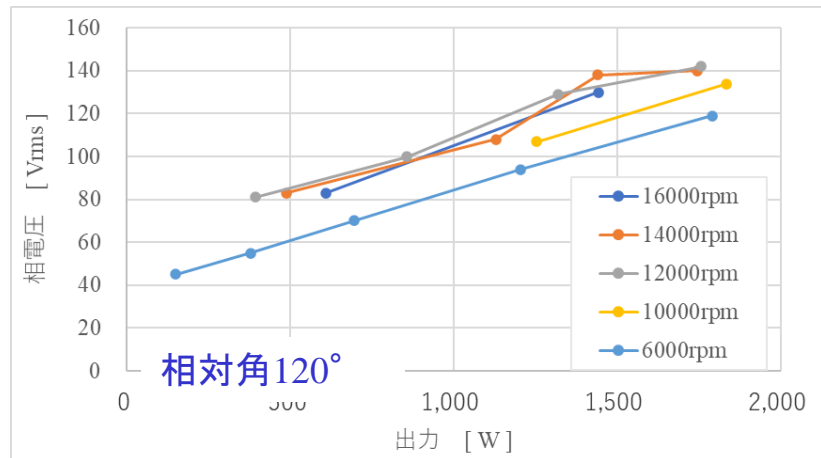
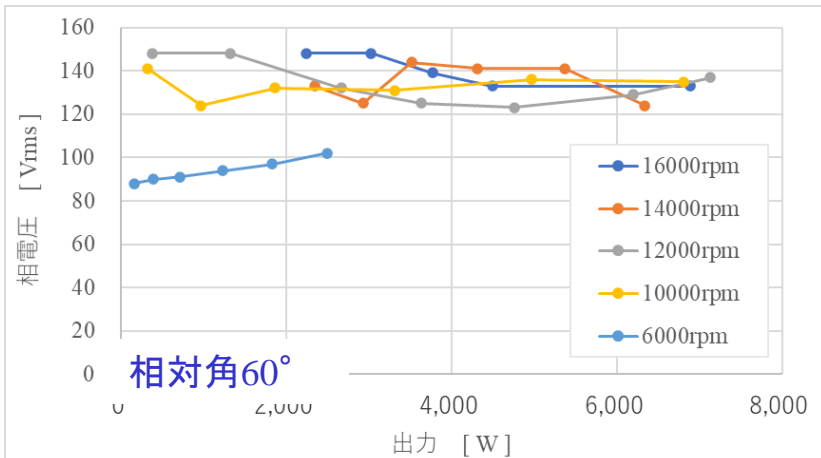
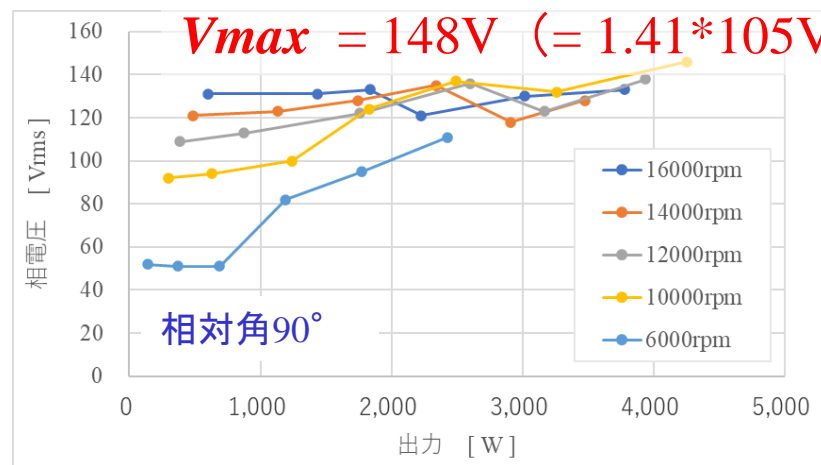
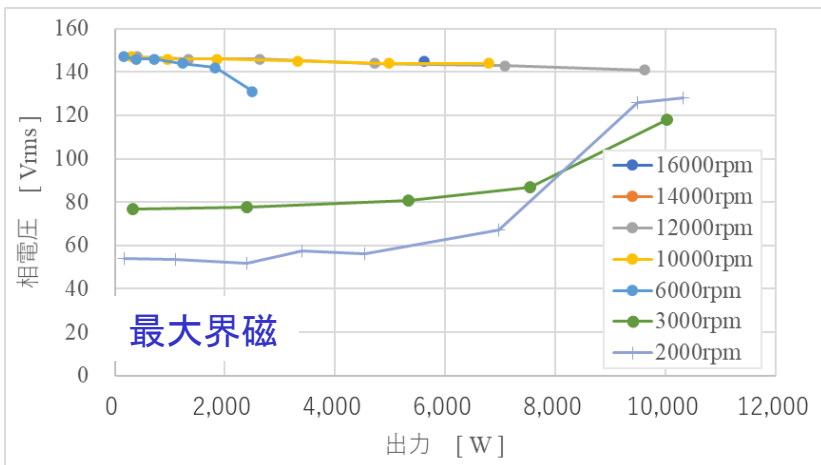
〔図 3.85〕 3相PWMインバータの構成

インホイールモータ原理と設計法、西山、遠藤、松田著、科学情報出版、p126

# 交直流電圧の検証

210VインバータのDC電圧を297Vとすれば、

$V_e$  [Vrms] =  $1/\sqrt{2} * V_{ad}$  [Vdc]/2 =  $0.35 * V_{ad}$  = 105V のはずだが、  
 (誘起電圧23.5Vrms/1000rpm, 負荷状態での電流波形は正弦波に近いことを確認)



つまり、DC電圧に対し、相電圧(rms)で半分、線間で87%程度で設計する。